



The Most Durable Automated Transmission



Contents





Overview

Because the DFTV based IVT can be so compact and light weight when durability is important the transmission size can be increased so that durability is increased.

The durability of the various transmission components in any form of transmission are very dependent on the quality of the fluid used in the transmission and the ability to keep the fluid clean and the ability to keep the fluids cool.

The Traction fluids used in CVT's are some of the best available and the inherent efficiency ensures the fluid is not thermally stressed. The filter system and oil circulation in a CVT ensures the fluid is kept exceptionally clean. Typical CVT's require oil changes at around more than 200,000 kms.

The friction clutches in a non IVT transmission are subject to high contact speeds as the transmission steps through the required ratios. High speeds create wear within the clutch plates and are a source of pollution of the lubricants.

In an IVT transmission the contact speeds of the clutch plates is always low as there are no steps and no launching process requiring plates to slip over each other at high speed.

The durability of the CVT components is critical to the overall durability of a transmission using a CVT.





Nissan Experience

The Nissan NSK transmissions that were introduced into the first cars in 2000 have proven their durability performance in real automobile applications. Ultimate Transmissions research has revealed very few transmission failures in under 200,000 kms. The failures that did occur were almost always associated with the use of the wrong traction fluid. Of the rest, it was common for the thrust bearings not the discs and rollers to fail.

The design life of an NSK CVT was 400,000 kms. The calculations made to ensure this design life were based on conventional bearing life calculations taking into account the fact that exceptionally pure steel as being used, and typical passenger vehicle duty cycles.



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Torotrak Experience

Torotrak state^{*} that they base the CVT life on 380 million cycles at 2.1 GPa for calculating design life. This equates to a maximum contact stress of 3.15GPa. When a Torotrak variator is operating in low gear at maximum input torque the maximum design stress under the (inner) contact point is 4.2GPa.

Nissan/NSK limit their maximum stress to 3.95 GPa or a Mean stress of 2.63GPa.

A more recent Torotrak paper expresses the following view of roller and disc durability.

The most recent development is the results from extended testing at lower contact stresses in the area of ~ 2.0 GPa mean Hertzian contact stress. Here, a number of test results have been produced with fatigue life extending well beyond the 12th power prediction. This leads to the potential for extended (if not potentially infinite) life of the variator below a contact stress threshold – see figure 14.

The impact is extended durability and, in conjunction with powersplit transmission architectures, further downsizing of the variator and hence transmission.



It can be seen from this diagram that most of the duty is associated with very low wheel torque and low speed. In this condition Ultimate Transmission estimates the Mean contact stresses as being less than 1GPa. In this condition a life exceeding 3,800 million cycles is expected. At 40 kms/hr. this equates to over 1,500,000 kms.



Figure 9 - Small front Wheel Drive Car Duty Cycle 160,000 kms.

* Extract from paper presented by Torotrak (Development) Ltd. Jtekt Corp & Shell Global Solutions to the JSME International Conference on Motion and Power Transmissions May 13-14, 2009 Matsushima Resort Japan entitled "FULLOTOROIDAL TRACTION DRIVE HIGH TEMPERATURE DURABILITY" By Dr Adrian Lee, Dr Andrew Hillsden, Yoshihiro Ono and Dr Stephen Evans.

Figure 9. Extract from Paper by Torotrak (Development) Ltd."Full Toroidal Traction Drives for Front Wheel Drive Applications" by Chris Brockbank & Dave Burtt 2006

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DFTV Durability

Ultimate Transmission's designs for the DFTV variator limit the maximum Hertzian stresses to 3.95GPa (Mean 2,63GPa) which is more in line with the NSK limits.

	Th													ARIATOR DOUB		-	
The following model can be used to calculate						i) ille ll	aximum sp	m losses,	z) me ma	kimum rau	o, o) Mecha	anicai voiu	me 4) Maximi	um input torque. :	b) Estimate	ea weigni	
Primrary inputs are shown as						Secondary	inputs from	Hertzian cont	act calculator are shown as					Calculated	Outputs		
INPUTS					1/10												
	entre of Toro			R,	RAR	RR	67.07			INPUT RPM					RPM		
Transverse radius of Toroid			R	50.92		Width of cor				W1		5 mm.					
Wheel inclin						а	21.70		Width of cor				W2		mm.		
Radius of roller			88	r1	24.80		OUTPUT RPM						RPM	0.42675328			
Primrary rotation angle				Α	31.95			ROLLER RPN					RPM	25.20	m/sec		
Radius of crown of roller			500		38.70			TOTAL RATIO				5.49					
Conformity of wheel to cavity			23		76.00		Area of inner contact point						l sq.mm				
Length of input contact point			L1		mm.	Maximum H						Gpa		check out			
Number of wheels					rollers			point from H	lertzian table		49,514	· · · · · · · · · · · · · · · · · · ·	49,314	49,69			
Number of cavities							Traction coet					0.055					
Length of o	utput contac			@ 39-deg. rotation		L2	3.2016				on roller beari			5,447			
	R1	R2	R3	r1	r2	r3		Sin A	Cos A	Sin a			Total clamping fo				
	40.121146	1469 44.3014173 35.9408765 24.7986 26.		986 26.6202	22.9770)	0.529179 0			6 0.92913257	1.38			output cont	act	3.	
	X1	X2 X3 r1 x2		x3		Sin A	Cos A	Sin a	Cos a		Overall radius of transmission without actuator				107.0		
	94.014853	97.9843536	5 90.04535	26 24.79	26.5283	23.0689)	0.529179	0.84851021				insmission without hydraulics				
										Overall length between outside of discs			122.2				
							Speed dif	% loss		Spin for this position			MAXIMUM INPUT TORQUE			spin	
Speed at	R1	1,511,765	5	r1	1,511,765	mm/minute	0						4	37.05	Nm		
Speed at	R2	1,669,277	7	r2	1,622,812	2	46,465	3.07%		5.8	33%						
Speed at	R3	1,354,252	2	r3	1,400,717	,	-46,465	3.07%		ES	TIMATED MA	ASS	ESTIMA	TED VOLUME			
										35	.05	kg		7.15	litres		
Speed at	X1	1,511,765	5	r1	1,511,765	5	0			% of SFTV			4.40 Disc	s and rollers only	litres	torque density	99.34031
Speed at	X2	1,575,595		x2	1,617,213		-41,619	2.75%				KW			,		
Speed at			x3	1,406,316			2.75%					274.58					
opeedat	7.5	1,447,555	1	^ 5	1,400,510	, 	41,015	2.7570		SPIN LOSSE	s		-	74.50			
CALCULATION OF APPARENT RADIUS OF CONTACTING POINTS											"L" position			5.83%	ENERGY LO	ST TO SPIN	
Angle of inclination of circle of contact of toroidal disc						A	31.95 deg			Spin loss in "LM" position			3.58%		2.23% factor		0.67
Angle of inclination of circle of contact of roller					а	21.70 deg			Spin loss in "C" position			0.00%		ENERGY LOST TO BEARING			
Radius of input circle of contact on toroidal disc						75.82 mm.			Spin loss in "HM" position			3.19%	0.00%				
Radius of output circle of contact of toroidal disc						-177.66 mm.			Spin loss in "H" position			7.17%	TOTAL LOSS				
Radius of contact of (toroidal) roller surface					26.69	mm.		Average sp				3.30%	2.23%				
										VAL CAVITIES		4.45 litres					

The extended life available from properly designed rolling contacts combined with the limited use of gears and clutches and associated lower parts count all go to verifying the superior life expectations of a DFTV - IVT.

The DFTV - IVT can remain smaller and more efficient than other transmission designs while maintaining greater life expectancy.



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